

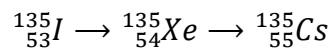
Nuclear energy – Quiz 2

Solutions

14-10-2019

1. Neutron poisons (12 pts)

I-135 and Xe-135 are produced as fission fragments in a nuclear reactor. Assume that I-135 is only formed as the result of a fission event and that its microscopic absorption cross section is negligible. Xe-135 is produced directly by fission and indirectly by the decay of I-135. The half-lives of I-135 and Xe-135 are 6.57 h and 9.10 h, respectively.



- a. Write the equations for the rate of change in concentration for I-135 $\left(\frac{dI}{dt}\right)$ and Xe-135 $\left(\frac{dXe}{dt}\right)$. (3 pts)

Solution

$$\frac{dI}{dt} = \gamma_I \Sigma_f \phi - \lambda_I I$$

$$\frac{dXe}{dt} = \gamma_{Xe} \Sigma_f \phi + \lambda_I I - \lambda_{Xe} Xe - \sigma_a^{Xe} Xe \phi$$

- b. The equilibrium concentration of I-135 is $2.6 \cdot 10^{15}$ atoms/cm³. Give the expression of the I-135 concentration at equilibrium and determine the value of the neutron flux (in cm⁻².s⁻¹). (3 pts)

$$\gamma_I = 0.0638$$

$$\gamma_{Xe} = 0.0025$$

$$\sigma_a^{Xe} = 3.20 \cdot 10^{-18} \text{ cm}^2$$

$$\Sigma_f = 0.002 \text{ cm}^{-1}$$

Solution

At equilibrium:

$$\frac{dI}{dt} = 0 \Rightarrow \gamma_I \Sigma_f \phi = \lambda_I I \Rightarrow I = \frac{\gamma_I \Sigma_f \phi}{\lambda_I} \Rightarrow \phi = \frac{\lambda_I I}{\gamma_I \Sigma_f}$$

$$\lambda_I = \frac{\ln 2}{T_{1/2}} = \frac{\ln 2}{6.57 * 3600} = 2.93 \cdot 10^{-5} \text{ s}^{-1}$$

The neutron flux is:

$$\phi = \frac{2.93 \cdot 10^{-5} \text{ s}^{-1} \times 2.6 \cdot 10^{15} \text{ cm}^{-3}}{0.0638 \times 0.002 \text{ cm}^{-1}} = 5.97 \cdot 10^{14} \text{ cm}^{-2} \cdot \text{s}^{-1}$$

- c. Determine the value of the xenon concentration at equilibrium. (2 pts)

Solution

At equilibrium:

$$\frac{dXe}{dt} = 0 \Rightarrow \gamma_{Xe} \Sigma_f \phi + \lambda_I I = \lambda_{Xe} Xe + \sigma_a^{Xe} Xe \phi \Rightarrow Xe = \frac{\gamma_{Xe} \Sigma_f^{fuel} \phi + \lambda_I I}{\lambda_{Xe} + \sigma_a^{Xe} \phi}$$

$$\lambda_{Xe} = \frac{\ln 2}{T_{1/2}} = \frac{\ln 2}{9.1 * 3600} = 2.12 \cdot 10^{-5} \text{ s}^{-1}$$

$$Xe = \frac{0.0025 \times 0.002 \text{ cm}^{-1} \times 5.97 \cdot 10^{14} \text{ cm}^{-2} \cdot \text{s}^{-1} + 2.93 \cdot 10^{-5} \text{ s}^{-1} \times 2.6 \cdot 10^{15} \text{ cm}^{-3}}{2.12 \cdot 10^{-5} \text{ s}^{-1} + 3.2 \cdot 10^{-18} \text{ cm}^2 \times 5.97 \cdot 10^{14} \text{ cm}^{-2} \cdot \text{s}^{-1}} \\ = 4.1 \cdot 10^{13} \text{ cm}^{-3}$$

- d. Show that under steady state conditions, Xe-135 is predominantly removed by burnout rather than by β -decay. (4 pts)

Solution

The rate at which xenon is removed by β -decay is:

$$\lambda_{Xe} Xe = 2.12 \cdot 10^{-5} \text{ s}^{-1} \times 4.1 \cdot 10^{13} \text{ cm}^{-3} = 8.69 \cdot 10^8 \text{ cm}^{-3} \cdot \text{s}^{-1}$$

The rate at which xenon is removed by burnout is:

$$\sigma_a^{Xe} Xe \phi = 3.2 \cdot 10^{-18} \text{ cm}^2 \times 4.1 \cdot 10^{13} \text{ cm}^{-3} \times 5.97 \cdot 10^{14} \text{ cm}^{-2} \cdot \text{s}^{-1} = 7.83 \cdot 10^{10} \text{ cm}^{-3} \cdot \text{s}^{-1}$$

2. Reactivity in LWR (8 pts)

Consider a light-water reactor with the following characteristics:

$$\epsilon = 1.028; L_{FNL} = 0.886; f = 0.754; p = 0.813; L_{TNL} = 0.955; \eta = 2.021$$

- a. A population of 15,000 neutrons exists at the beginning of a generation. Calculate the number of neutrons absorbed in the fuel and in the resonance peaks. (4 pts)

Solution

The multiplication factor is equal to

$$k = \frac{N}{N_0} = \epsilon L_{FNL} p L_{TNL} f \eta$$

The number of neutrons absorbed in the fuel is

$$N = N_0 \epsilon L_{FNL} p L_{TNL} f = 15000 \times 1.028 \times 0.886 \times 0.813 \times 0.955 \times 0.754 = 7998$$

Number of neutrons absorbed by the resonance peaks:

$$N = N_0 \epsilon L_{FNL} (1 - p) = 15000 \times 1.028 \times 0.886 \times (1 - 0.813) = 2554.8$$

- b. What is the effect of an increase in the fuel's temperature on the factors of the 6-factor formula? How does such a change affect the reactivity? (4 pts)

Solution

Raising the temperature of the fuel causes the uranium nuclei to vibrate more rapidly within their lattice structures. Vibrating nuclei moving towards or away from the neutron can increase the absorption rate of the neutron with slightly lower or higher energy than the resonance one. Therefore, raising the temperature causes a broadening of the energy range of neutrons that may be resonantly absorbed in the fuel. The broadened resonances result in a larger percentage of neutrons having energies allowing their capture in the fuel pellets.

This results mainly in a reduction of the resonance escape probability p and a decrease in reactivity.

3. Diffusion of neutrons (10 pts)

A critical and uniform spherical reactor with a diameter of 7.6 m has the following properties:

$$\nu = 2.43; D = 1.01 \text{ cm}$$

The material inside the reactor has an atomic mass of 270 and a density of 9.4 g/cm^3 .

The average neutron flux is $2.1 \cdot 10^{12} \text{ cm}^{-2} \cdot \text{s}^{-1}$ and the total absorption rate is $1.931 \cdot 10^{18} \text{ s}^{-1}$.

The Avogadro number is $N_A = 6.022 \cdot 10^{23} \text{ mol}^{-1}$.

- a. Determine the values of the macroscopic and microscopic absorption cross sections. (4 pts)

Solution

The absorption reaction rate is given by

$$R = \Sigma_a \phi V = \Sigma_a \phi \frac{4}{3} \pi r^3$$

$$V = \frac{4}{3}\pi \left(\frac{760}{2}\right)^3 = 2.3 \cdot 10^8 \text{ cm}^3$$

The macroscopic cross section is

$$\Sigma_a = \frac{R}{\phi V} = \frac{1.931 \cdot 10^{18} \text{ s}^{-1}}{2.1 \cdot 10^{12} \text{ cm}^{-2} \text{ s}^{-1} \times 2.3 \cdot 10^8 \text{ cm}^3} = 0.0040 \text{ cm}^{-1}$$

The microscopic cross section is

$$\sigma_a = \frac{\Sigma_a}{N}$$

The number of nuclides in the reactor is

$$N = \frac{\rho \times N_A}{M} = \frac{9.4 \frac{\text{g}}{\text{cm}^3} \times 6.022 \cdot 10^{23} \text{ mol}^{-1}}{270 \frac{\text{g}}{\text{mol}}} = 2.09 \cdot 10^{22} \text{ cm}^{-3}$$

Therefore, the microscopic absorption cross section is

$$\sigma_a = \frac{0.0040 \text{ cm}^{-1}}{2.09 \cdot 10^{22} \text{ cm}^{-3}} = 1.91 \cdot 10^{-25} \text{ cm}^2 = 0.191 \text{ barn}$$

b. Calculate the buckling. (2 pts)

Solution

The buckling for a spherical reactor is given by

$$B^2 = \left(\frac{\pi}{r}\right)^2 = \left(\frac{\pi}{380}\right)^2 = 6.83 \cdot 10^{-5} \text{ cm}^{-2}$$

c. Determine the value of the macroscopic fission cross section. (2 pts)

Solution

The reactor is critical and the multiplication factor can be written as

$$k = 1 = \frac{\nu \Sigma_f}{\Sigma_a + DB^2}$$

Therefore, the macroscopic fission cross section is

$$\Sigma_f = \frac{\Sigma_a + DB^2}{\nu} = \frac{0.0040 \text{ cm}^{-1} + 1.01 \text{ cm} \times 6.83 \cdot 10^{-5} \text{ cm}^{-2}}{2.43} = 0.0017 \text{ cm}^{-1}$$

d. Calculate the total power in the reactor in MW considering that the energy released by one fission event is $E_f = 200 \text{ MeV}$. (2 pts)

$$1 \text{ MeV} = 1.602 \cdot 10^{-13} \text{ J and } 1 \text{ W} = 1 \text{ J/s}$$

Solution

The total power is equal to the average energy generated per fission \times average fission rate \times volume:

$$\begin{aligned}
P &= E_f \times \Sigma_f \phi \times V \\
&= 200 \text{ MeV} \times 1.602 \cdot 10^{-13} \text{ J} \times 0.0017 \text{ cm}^{-1} \times 2.1 \cdot 10^{12} \text{ cm}^{-2} \text{ s}^{-1} \times 2.3 \cdot 10^8 \text{ cm}^3 \\
&= 26.31 \text{ MW}
\end{aligned}$$

Possibly useful equations

$$N \left(\frac{\text{atoms}}{\text{cm}^3} \right) = \frac{\rho \left(\frac{\text{g}}{\text{cm}^3} \right) N_A \left(\frac{\text{atoms}}{\text{mole}} \right)}{M \left(u = \frac{\text{g}}{\text{mole}} \right)} ; \quad \Sigma \left(\text{cm}^{-1} \right) = N \left(\frac{\text{atoms}}{\text{cm}^3} \right) \sigma \left(\text{cm}^2 \right)$$

$$R_{\text{reaction}} \left(\frac{\text{reactions}}{\text{cm}^3 \times \text{s}} \right) = \phi \left(\frac{\text{neutrons}}{\text{cm}^2 \times \text{s}} \right) \times \Sigma_{\text{reaction}} \left(\text{cm}^{-1} \right) ; \quad T_{1/2} = \frac{\ln 2}{\lambda}$$

$$k = \varepsilon L_{FNL} p L_{TNL} f \eta ; \quad k_{\infty} = \frac{\nu \Sigma_f}{\Sigma_a} ; \quad B^2 = \frac{\nu \Sigma_f - \Sigma_a}{D}$$

$$k = \frac{\nu \Sigma_f}{\Sigma_a + DB^2} ; \quad P = E_f R_f V$$

Geometry	Dimensions	Buckling B^2	Flux	A
Rectangular parallepiped	a x b x c	$\left(\frac{\pi}{a}\right)^2 + \left(\frac{\pi}{b}\right)^2 + \left(\frac{\pi}{c}\right)^2$	$A \cos\left(\frac{\pi}{a}x\right) \cos\left(\frac{\pi}{b}y\right) \cos\left(\frac{\pi}{c}z\right)$	$3.87 \frac{P}{V E_f \Sigma_f}$
Finite cylinder	Radius R, height H	$\left(\frac{2.405}{R}\right)^2 + \left(\frac{\pi}{H}\right)^2$	$A J_0\left(\frac{2.405 r}{R}\right) \cos\left(\frac{\pi z}{H}\right)$	$3.63 \frac{P}{V E_f \Sigma_f}$
Sphere	Radius R	$\left(\frac{\pi}{R}\right)^2$	$A \frac{1}{r} \sin\left(\frac{\pi r}{R}\right)$	$\frac{P}{4R^2 E_f \Sigma_f}$